



A Novel Three-Port Converters For Solar Power System

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Abstract: The conventional three-port power converters with bridge rectifiers are inefficient and may not be practical for the low-voltage micro generators. This paper presents an efficient ac-to-dc power converter that avoids the bridge rectification and directly converts the low ac input voltage to the required high dc output voltage at a higher efficiency. The proposed converter consists of a boost converter in parallel with a buck–boost converter, which are operated in the positive half cycle and negative half cycle, respectively. Detailed analysis of the converter is carried out to obtain relations between the power, circuit parameters, and duty cycle of the converter. Based on the analysis, control schemes are proposed to operate the converter. Design guidelines are presented for selecting the converter component and control parameters. A self-starting circuit is proposed for independent operation of the converter. Detailed loss calculation of the converter is carried out. Simulation results are presented to validate the proposed converter topology and control schemes.

Keywords: AC–DC conversion, boost converter, energy harvesting, low power, low voltage, power converter control.

Introduction: The future of this earth and mankind substantially depends on our ability to slow down the population increase in the “Third World” by civilized means. The key is to increase the standard of living, to overcome the inhumane poverty and deprivation. Development requires mechanization and energy. Energy consumption increases proportionally to the gross national product or prosperity while simultaneously the population growth will decrease exponentially. Many developing countries possess hardly any energy sources and their population doubles every 15- 30 years. The result of which are commonly known that is civil wars and

fundamentalism. If these developing countries are provided with only a humane and viable minimum of energy the global energy consumption will drastically increase. The sun is the only source which can supply such an enormous amount of energy without an ecological breakdown and without safety hazards and without a rapid depletion of natural resources at the expenses of future generations. Solar chimneys are such devices which can generate energy up to large extent by use of the simple device that is greenhouse collector, Vertical chimney and turbine and produce electricity continuously at minimum cost. It is very necessary to adopt this technology in every part of the world like other conventional sources which we are using regularly.



Figure 1: Block Diagram

Different topologies like multiport converters [4], multiport power electric interface [2] etc. are done by researchers earlier. But this is not an integrated solution since only a few devices are shared. Some TPCs are constructed from full-bridge, half bridge, or series-resonant topologies by utilizing the magnetic coupling through a multilinking transformer [8]-[9]. However, too many active switches have been used, resulting in a complicated driving and control circuit, which may degrade the reliability and performance of the integrated converters. Some three port converters like boost-integrated TPC [10] developed from a phase-shift full-bridge converter (FBC) and a Integrated TPC [5]-[7] from a half-bridge Converter is to implement three-port interface. However, because the equivalent conversion circuit between the

input source and energy storage element is a step-up or step-down converter. With limited voltage conversion ratio, they are not flexible enough for applications where the voltage of the source port, such as solar, fuel cells and thermoelectric generator, varies over a wide range. We focus on full bridge three port converter which is buck boost integrated for both Buck and boost operations. It uses fewer components thereby achieves higher system efficiency.

A three port converter must feature single-stage conversion between any two of the three ports, higher system efficiency, fewer components, faster response, compact packaging, and unified power management among the ports with centralized control. For renewable energy harvesting systems, one of the toughest challenges for the power management circuits is that, the converter must be able to efficiently function with all existing wide source voltage conditions. This motivates the need of buck-boost integrated full bridge three port converters with wide input voltage range, higher system efficiency, and small physical size. ZVS of all the primary side

Switches can also be achieved with this FB-TPC.

2. Derivation OF the FB-TPC From a Full-Bridge DC-DC Converter

A systematic method for generating Three Port Converter topologies from Full Bridge Converters are described here. This systematic method is used to find a novel full bridge TPC(FB-TPC). This method splits the two switching legs of the FBC into two switching cells with different sources and allows a dc bias current in the transformer. A buck boost converter is integrated in the FB-TPC and used to configure the power flow path between the two ports on the primary side of the converter, which is aimed to handle a wide range of source voltage. ZVS of all the primary-side switches can also be achieved with this FB-TPC.

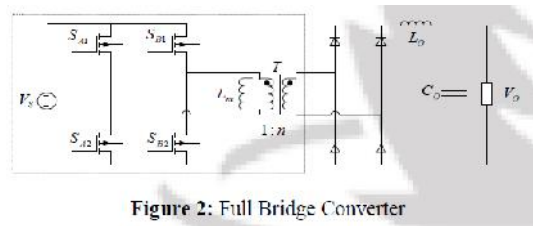


Figure 2: Full Bridge Converter

Referring to Fig.2, the primary side of the FBC consists of two switching legs, composed of SA1, SA2 and SB1, SB2 in parallel, connected to a common input source V_s . For the primary side of the FBC, the constraint condition of the operation of the FBC is the voltage-second balance principle of the magnetizing inductor L_m . This means that, from a topological point of view, the two switching legs of the FBC can also be split into two symmetrical parts, cells A and B, if only L_m satisfies the voltage-second balance principle, as shown in Fig.3.

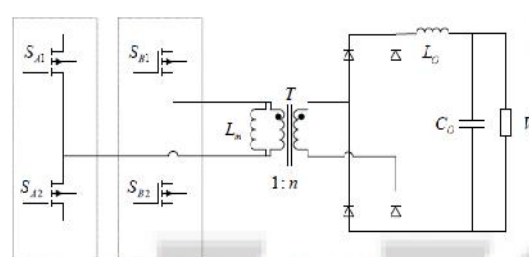


Figure 3: Two Switching Cells of Full Bridge Converter

The two cells can be connected to different sources, V_{sa} & V_{sb} respectively, as shown in Fig.4, and then a novel FB-TPC is derived. The voltage of the two sources of the FB-TPC can be arbitrary. Specially, if V_{sa} always equals V_{sb} , the two cells can be paralleled directly and then the conventional FBC is derived. Therefore, the FBC can be seen as a special case of the FB-TPC as shown in Fig.4.

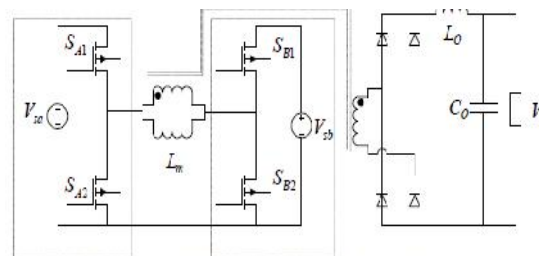


Figure 4: Full Bridge Three Port Converter

Close observation indicates that the FB-TPC has asymmetrical structure and both V_{sa} and V_{sb} can supply power to the load V_o . In addition, a bidirectional buck-boost converter [11] is also integrated in the primary side of the FBTPC by employing the magnetizing inductor of the transformer L_m as a filter inductor. With the bidirectional buck-boost converter, the power flow paths between the two sources, V_{sa} and V_{sb} , can be configured and the power can be transferred between

V_{sa} and V_{sb} freely. The unique characteristics of the FB-TPC are analyzed and summarized as follows.

1) The FB-TPC has two bidirectional ports and one isolated output port. Single-stage power conversion between any two of the three ports is achieved. The FB-TPC is suitable for renewable power systems and can be connected within input source and an energy storage element, such as the photovoltaic (PV) with a battery backup or with two energy storage elements, such as the hybrid battery and the super capacitor power system.

2) A buck-boost converter is integrated in the primary side of the FB-TPC. With the integrated converter, the source voltage V_{sa} can be either higher or lower than V_{sb} advice versa. This indicates that the converter allows the sources voltage varies over a wide range.

3) The devices of the FB-TPC are the same as the FBC and no additional devices are introduced which means high integration is achieved.

4) All four active switches in the primary side of the FBTPC can be operated with ZVS by utilizing the energy stored in the leakage inductor of the transformer, who seprinciple is similar to the phase-shift FBC.

3. FB-TPC for the Stand-Alone Renewable Power System

The FB-TPC, as shown in Fig.3, is applied to a stand-alone PV power system with battery backup to verify the topology. To better analyze the operation principle, the FB-TPC topology is redrawn in Fig.5, the two source ports are connected to a PV source and a battery respectively, while the output port is connected to a load.

There are three power flows in the standalone PV power system 1) from PV to load 2) from PV to battery and 3) from battery to load. As for the FB-TPC, the load port usually has to be tightly regulated to meet the load requirements, while the input port from the PV source should implement the maximum power tracking to harvest the most energy. Therefore, the mismatch in power between the PV source and load has to be charged into or discharged from the battery port, which means that in the FB-

TPC, two of the three ports should be controlled independently and the third one used for power balance. As a result, two independently controlled variables are necessary

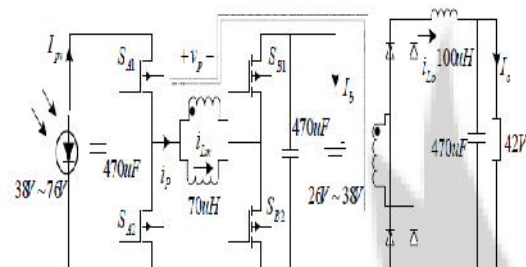


Figure 5: Topology of the FB-TPC

A. Switching state analysis Ignoring the power loss in the conversion, we have

$$P_{pv} = P_b + P_o$$

Where p_{pv} , p_b , and p_o are the power flows through the PV, battery and load port, respectively. The FB-TPC has three possible operation modes 1) dual-output (DO) mode, with $p_{pv} \geq p_o$ the battery absorbs the surplus solar power and both the load and battery take the power from PV (2) dual-input (DI) mode with $p_{pv} \leq p_o$ and $p_{pv} > p_o$, the battery discharges to feed the load along with the PV and (3) single-input single-output (SISO) mode with $p_{pv} = 0$, the battery supplies the load power alone. When $p_{pv} = 0$ exactly, the solar supplies the load power alone and the converter operate in a boundary state of DI or DO modes. This state can either be treated as DI or DO mode. Since the FB-TPC has a symmetrical structure, the operation of the converter in this state is the same as that of SISO mode, where the battery feeds the load alone. The operation modes and power flows of the converter are listed in Table I. The power flow paths/directions of each operation mode have been illustrated in Fig.6. The switching states in different operation modes are the same and the difference between these modes are the value and direction of i_{Lm} as shown in Fig.5, which is dependent on the power of p_{pv} and p_o .

Table 1: Operation Modes of the FB-TPC

Operation modes	Power of PV	Power of battery
Dual-output mode	$P_{pv} > p_o$	Battery charging, $p_b \geq 0$
Dual-input mode	$P_{pv} < p_o$, $P_{pv} > 0$	Battery discharging, $p_b < 0$
Single-input single-output mode	$P_{pv} = 0$	Battery discharging, $P_b = p_o$

In the DO mode, i_{Lm} is positive, in the SISO mode, i_{Lm} is negative and in the DI mode, i_{Lm} can either be positive or negative. Take the DO mode as an example to analyse.

For simplicity, the following assumptions are made: 1) C_{pv} , C_b and C_o are large enough and the voltages of the three ports, V_{pv} , V_b and V_o are constant during the steady state and 2) the $V_{pv} \geq V_b$ case is taken as an example for the switching state analysis.

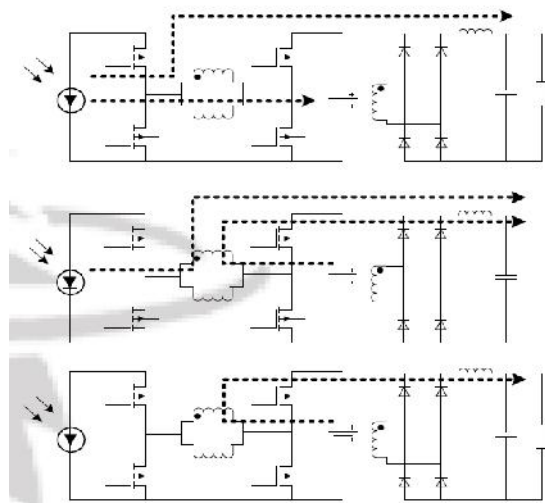


Figure 6: Power Flow Paths/Directions of each Operation Mode. (a) DO Mode. (b) DI Mode. (c) SISO Mode

There are four switching states in one switching cycle. The key waveforms are shown in Fig.11.

State I [0 t - 1 t]

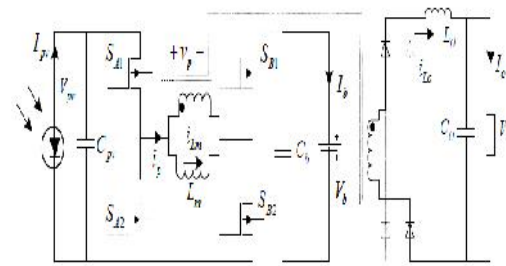


Figure 7: Equivalent Circuit of Switching State I [$t_0 - t_1$]

Before t_0 , S_{A2} and S_{B2} are ON and S_{A1} and S_{B1} are OFF, while i_{Lm} freewheels through S_{A2} and S_{B2} . At t_0 , S_{A1} turns ON and S_{A2} turns OFF. A positive voltage is applied across the transformer's primary winding

$$\begin{cases} \frac{di_{Lm}}{dt} = \frac{V_{PV}}{L_m} \\ \frac{di_{Lo}}{dt} = \frac{nV_{PV} - V_o}{L_o} \\ i_p = i_{Lm} + ni_{Lo} \end{cases}$$

State II [1 t - 2 t]

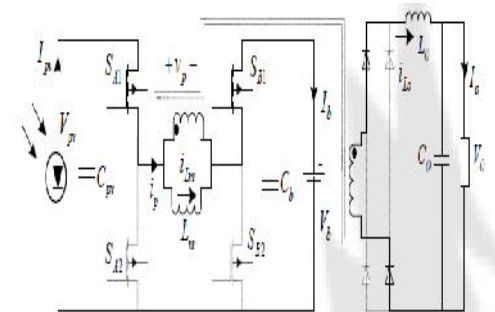


Figure 8: Equivalent Circuit of Switching State II [$t_1 - t_2$]

At t_2 , S_{B2} turns OFF and S_{B1} turns ON. A positive voltage is applied on the primary winding of the transformer.

$$\begin{cases} \frac{di_{Lm}}{dt} = \frac{V_{PV} - V_b}{L_m} \\ \frac{di_{Lo}}{dt} = \frac{n(V_{PV} - V_b) - V_o}{L_o} \\ i_p = i_{Lm} + ni_{Lo} \end{cases}$$

State III [2 t - 3 t]

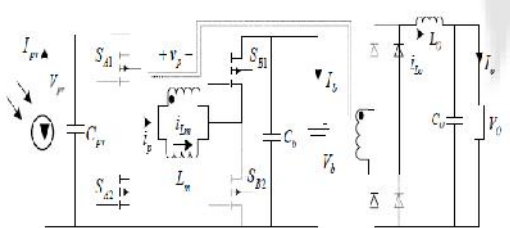


Figure 9: Equivalent Circuit of Switching State III [t₂ - t₃]

At t₂, SA1 turns OFF and SA2 turns ON. A negative voltage is applied on the primary winding of the transformer

$$\begin{cases} \frac{di_{Lm}}{dt} = -\frac{V_b}{L_m} \\ \frac{di_{Lo}}{dt} = \frac{nV_b - V_o}{L_o} \\ i_p = i_{Lm} - ni_{Lo} \end{cases}$$

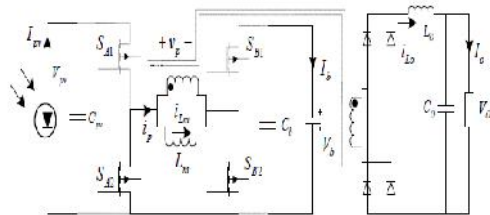


Figure 10: Equivalent Circuit of Switching State III [t₃ - t₄]

At t₃, SB1 turns OFF and SB2 turns ON. The voltage across the primary winding is clamped at zero and i_{Lm} freewheels through SA2 and SB2.

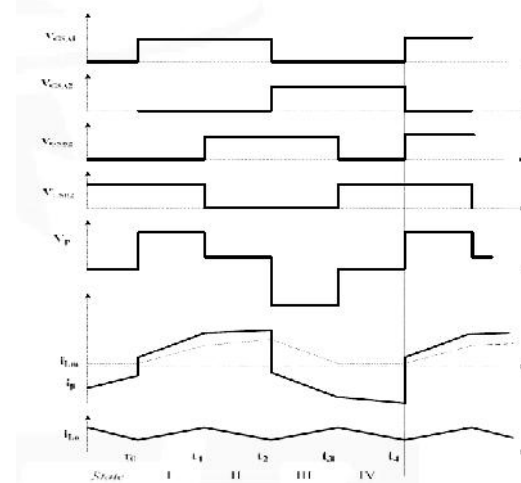


Figure 11: Key Waveforms of the FB-TPC

4. Simulation Results

Full bridge three port converter is simulated using MATLAB/SIMULINK. Simulink model of the Full Bridge Three Port Converter operating in dual output mode is shown in Fig.12. Simulation of the full bridge three port converter operating in dual output mode is done by using 38V DC from PV array as input. A regulated voltage, 57.7V DC is obtained at the output side. The magnetizing inductor of the transformer performs buck operation. In closed loop system, the output will be feedback through the controller to the input. Carrier based PWM is used for the closed loop operation. Here R load is used as the load in the closed loop circuit. Hence if there is any over distortion or variation in results, the PWM technique will give the feedback to input according to input varied. It gives better result compared to the open loop R load, because of stable result.

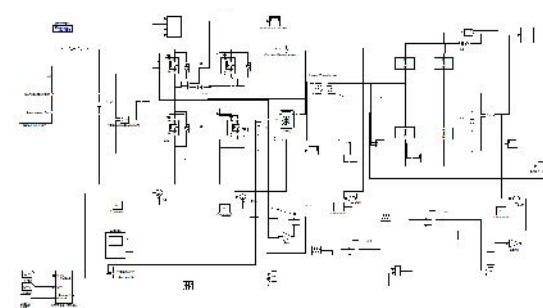


Fig.12 Proposed model

In DO mode, the battery absorbs the surplus solar power and both the load and battery take the power from PV. It can be seen that, the output

voltage, current and power of the converter are 42V, 4.3A and 180W respectively.

Input Voltage $V_{in} = 38V$ DC



Output voltage $V_{out} = 57.7V$



Output power



5. Conclusion

A Full-bridge converter generated with Three-port Full-bridge has been presented in this paper. A carrier based PWM control method is applied to the Three-port Full-bridge converter. This converter offers the advantages of simple topologies and control, reduced number of devices and a Single-stage power conversion between any two of the three ports. They are suitable for renewable power systems that are sourced by solar, thermoelectric generator etc with voltages varying over a wide range. Full bridge three port converter is simulated using MATLAB/SIMULINK validating the effectiveness of the converter and its control scheme. A 57.7VDC constant output is obtained for input voltage range 38V DC.

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